

METAL FLOW ANALYSIS IN STREAMLINED EXTRUSION DIES USING DEFORM

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Abstract- Extrusion dies are presently modified as streamlined extrusion dies. In these dies the smooth flow of metal is ensured and hence formation of dead metal zone is avoided. In this paper an attempt is made to analyze the variation of velocity components (V_x , V_y , V_z) and strain rate components (ϵ_x , ϵ_y , ϵ_z) of the extruded metal along the die length. The analysis is done for the streamlined extrusion dies designed based on the third order polynomial equation. The analysis is also carried out for various reduction ratios.

Keywords – Extrusion dies, Velocity, Strain rate and Third order Polynomial equation

1. INTRODUCTION

Metal extrusion is widely carried out using shear dies. But the shear faced extrusion dies [1] suffer from more redundant work attributed to formation of dead metal zone. Dead metal zone results from the resistance offered by the die surface to the extruded metal. Extrusion dies are presently modified as streamlined extrusion dies. Fig. (1). In these dies [2] the smooth flow of metal is ensured and hence formation of dead metal zone is avoided. This results in reduced extrusion pressure for the given reduction ratio. In this paper an attempt is made to analyze the variation of velocity components (V_x , V_y , V_z) and strain rate components (ϵ_x , ϵ_y , ϵ_z) of the metal getting extruded along the die length with the help of computer. The analysis is done for the streamlined extrusion dies designed based on the third order polynomial equation. The analysis is also carried out for various reduction ratios.

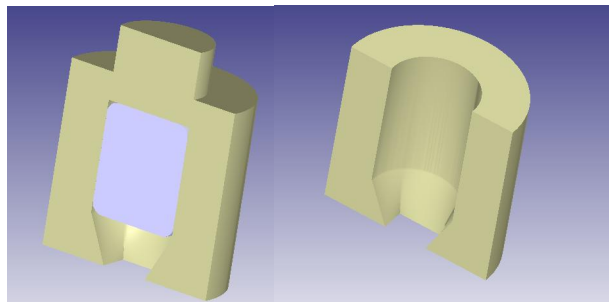


Figure.1. Streamlined Extrusion Dies

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II. VELOCITY

The following assumptions are required to construct the kinematically admissible velocity field [3] for the extrusion of regular polygonal sections from cylindrical billets.

The material of the billet passing through sector OEG at the die entry goes through triangular LFH at the die exit, preserving the extrusion (or the drawing ratio).

Stream surface OEFL consists of a number of curved streamlines, which start from a point (say E') at the entry and end at a corresponding point (say F') at the exit maintaining the proportionality of the position.

Any coordinate along streamline E' F' is formulated in a Cartesian coordinate system as follows.

$$\begin{aligned} X &= f_1(z) = b_1z^3 + b_2z^2 + b_3z + b_4 \\ Y &= f_2(z) = c_1z^3 + c_2z^2 + c_3z + c_4 \\ Z &= z \end{aligned} \quad \dots\dots\dots (1)$$

Where b_i and c_i ($i=1, 2, 3$ and 4) are constants, determined by the boundary conditions. Consider that this streamline does not produce any abrupt change of flow direction along the extrusion axis at the entry and the exit of die. The boundary conditions are given for equation (1) as

$$\begin{aligned} & \left. \begin{aligned} X &= n \sin \phi, \quad \frac{\partial x}{\partial z} = 0 \\ y &= n \cos \phi, \quad \frac{\partial y}{\partial z} = 0 \end{aligned} \right\} \text{at } z = 0 \\ & \left. \begin{aligned} x &= \frac{n}{Ro} a \tan \psi, \quad \frac{\partial x}{\partial z} = 0 \\ y &= \frac{n}{Ro} a, \quad \frac{\partial y}{\partial z} = 0 \end{aligned} \right\} \text{at } z = L \end{aligned} \quad \dots\dots\dots(2)$$

Where

$$\tan \psi = \frac{N}{\pi N} \tan \left[\frac{\pi}{N} \right] \cdot \phi$$

=cφ

Where Ro is the radius of billet, 'a' is the half-side length of product cross-section, N is the number of sides in regular polygon, L is the length of die, n is the distance from the axis to an arbitrary point E' at the die entry, and ϕ

and ψ are the angles between the plane of symmetry and the stream surface at entry and exit of the die respectively. Substitution of these boundary conditions into equation (1) gives.

$$\begin{aligned}
 X &= n \sin \phi + n \left[\frac{a}{R_0} - \frac{c \phi - \sin \phi}{3} \right] L \left[\frac{z}{-2} \right]^2 L \left[\frac{z}{3} \right]^3 \\
 y &= n \cos \phi + n \left[\frac{a}{R_0} - \frac{c \phi}{3} \right] L \left[\frac{z}{-2} \right]^2 L \left[\frac{z}{3} \right]^3 \\
 z &= z
 \end{aligned} \tag{3}$$

Assuming that the plastically deforming zone is bounded by shear planes at the entry and the exit of die, and utilizing the determinant of the Jacobean of equation (3), the velocity components for incompressible material are determined as

$$\begin{aligned}
 V_x &= \frac{n \left[\frac{a}{R_0} - \frac{c \phi - \sin \phi}{3} \right] f'(z)}{g(\phi, z)} \cdot V_0 \\
 V_y &= \frac{n \left[\frac{a}{R_0} - \frac{c \phi}{3} \right] f'(z)}{g(\phi, z)} \cdot V_0 \\
 V_z &= \frac{1}{g(\phi, z)} \cdot V_0
 \end{aligned} \tag{4}$$

Where

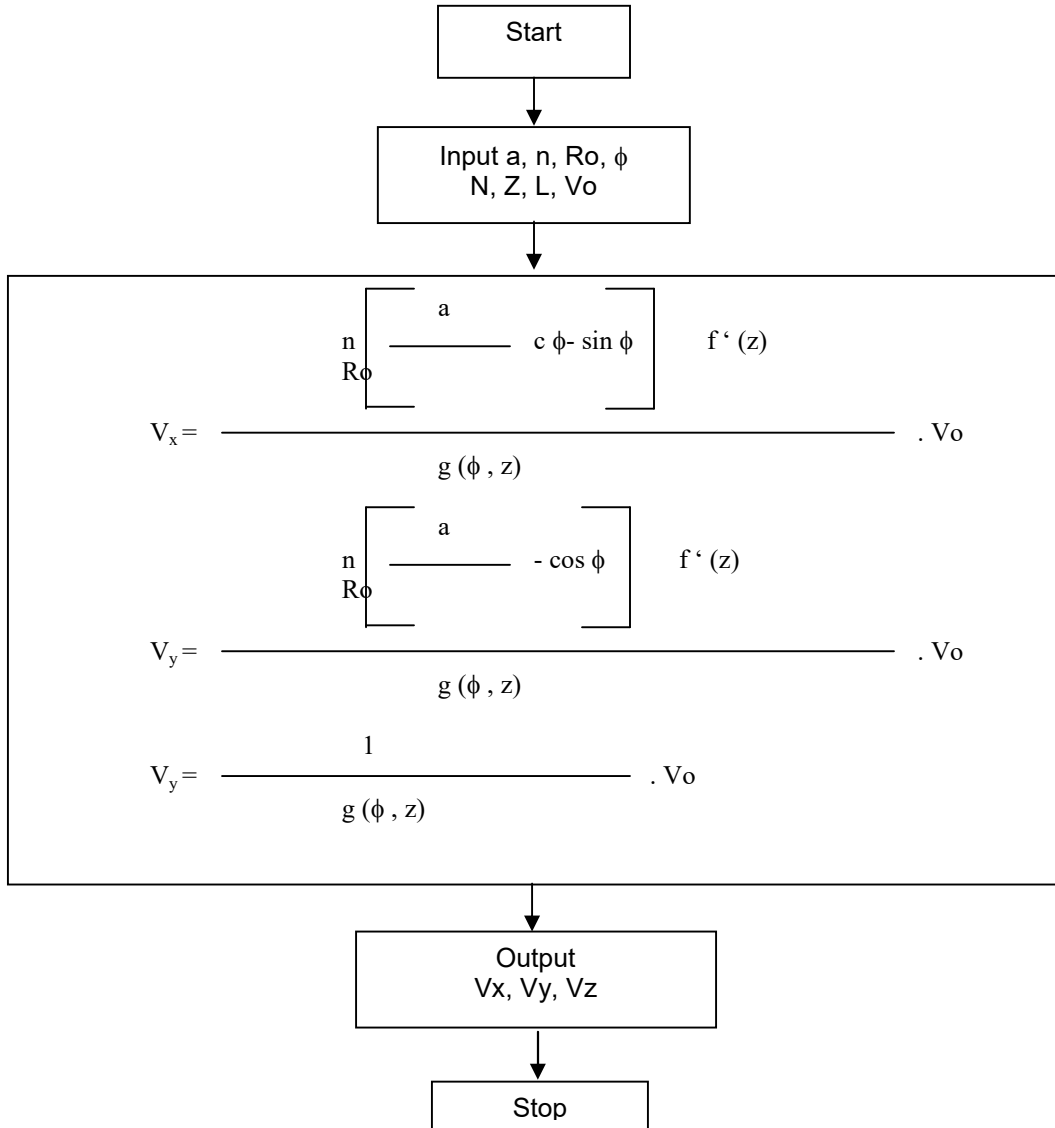
$$\begin{aligned}
 g(\phi, z) &= \left[(1-f) + \frac{c}{R_0} \left[\frac{a}{f} \right]^2 \right]^2 \\
 &+ \left[\frac{(1+c)(1-f)}{R_0} - \frac{a}{f} \cos \phi + c(1-f) \right] \left[\frac{a}{R_0} - \frac{c \phi - \sin \phi}{3} \right]
 \end{aligned}$$

III. COMPUTER PROGRAM FOR THE CALCULATION OF VELOCITY COMPONENTS

(V_x, V_y, V_z)

Computer program is developed for the calculation of velocity components values (V_x, V_y, V_z) for various reduction ratios by changing the following parameter.

- (i) Reduction ratio (ii) Position along the die length (iii) arbitrary radius at the inlet of the bullet and
- (iv) Sweep angle. The flow chart for the program is given below.



IV. RESULTS AND DISCUSSION

VELOCITY

Metal flow analysis using velocity field has been done for the reduction ratios of 70% and 80% for extruding circular rod into a square shape. The following inferences can be made.

When the reduction ratio is 80%, V_x and V_y components remains zero along the length of the die when the sweep angle is zero. The V_z component steeply increases for all the reduction ratios. V_x remains zero along the length of the die. V_y value decreases to the negative ordinate and then attains zero at the die exit. V_z component gradually increases and attain of maximum value at the die exit. In general, when the sweep angle remains zero, the velocity component along the X direction for all the values of the radius of the billet is zero. However, velocity component along the Y direction initially attains negative value and then becomes zero at the die exit. While the V_z component gradually increases and then attains its peak at the die exit.

When the reduction ratio decreases to 70%, it is observed that the velocity components V_x , V_y and V_z respond in the same way; but the peak value of V_z is lower when compared to larger reduction ratio. When the sweep angle value is changed to 15° , it is observed that both V_x and V_y components take negative value along the die length and then attain zero at the die exit while the V_z component gradually increases and attains peak at the die exit.

When the sweep angle is change to 30° , it is observed that V_x , V_y and V_z components respond in the same way as mentioned in the case of sweep angle of 15° , but the negative peek value of V_x increases. However, the negative peek of V_y decreases. There is no change in the value of V_z component for both the values of sweep angle.

When the reduction ratio decreases to 70%, it is observed that the velocity components V_x , V_y and V_z respond in the same way, but the peak value of V_z is lower when compared to larger reduction ratio.

When the sweep is increases to 45° , the V_x and V_y components take equal negative values along the length of the die and attain zero at the die exit. V_z gradually increases and takes maximum value at the exit.

STRAIN RATE

It is observed that the strain rate ϵ_z initially decreases with the die length and then increases as shown in Fig. (2). The ϵ_x and ϵ_y components remain zero along the length of the die for all the values sweep angle, when the radius is zero.

When the radius increases to 10 mm maintaining the sweep angle as zero, the strain rate along the Z axis initially decreases and then increases, but the peek strain rate value along the Z direction is more when compared to the strain rate for the radius of zero at the entry.

The ϵ_z components is steeper for higher reduction ratios, when compared to lower reduction ratios.

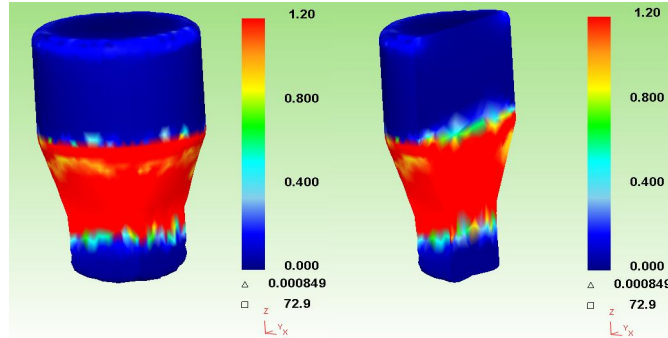


Figure.2-Strain rate in Dies during extrusion

V. CONCLUSIONS

It is concluded that the V_x and V_y components attain negative value and then goes to zero at the die exit when the metal is getting extruded through the die. But the V_z component always increases with the die length. The rate of increase of V_z is more for larger reduction ratios. Strain rate along the Z axis initially decreases and then increases.

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